

## ANALYSIS OF COMPLEX NONLINEAR DYNAMIC SYSTEMS BY MEANS OF PARTIAL MODELS. CONVERGENCE OF ITERATIVE PROCEDURES

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Problems of iterative convergence in the analysis of complex dynamic systems with the use of partial models are dealt with. Nonlinear systems are considered. An example of some nonlinear system and the suitable iteration process are presented. The time analysis is also dealt with. On the assumption that the solutions of the system can be expanded in power series with respect to a small parameter, the general condition of convergence is formulated. Limitations for the successive derivatives of nonlinear stiffness characteristics are determined as a consequence of the convergence conditions of the procedures.

### 1. INTRODUCTION

Growing demand to lower the level of noise, vibrations and to increase the durability of the machinery make the researchers create and analyze some more and more complex dynamic models of these machines. Current computational techniques, used both to calculate and to measure, make it possible to construct models of several scores or even hundreds of degrees of freedom and take into account various nonlinearities of the system under consideration. However, the use of such complicated models creates certain difficulties. Identification of a large number of parameters entering the models is both cumbersome and expensive. Interpretation of the results obtained is not an easy task. The calculation procedure may appear difficult and probability increases of making "unfriendly" errors in the computational procedures that are very difficult to discover. Those difficulties vanish when some simpler models are employed.

In the paper [2] a concept of an analysis of complex dynamic systems with the use of partial models was put forward. It makes it possible to preserve a high degree of complexity of vibration phenomena and, at the

same time, to use relatively simple computational means. The main idea behind this method is as follows:

- a full model (a complex one) is split up into partial (simpler) models by using an analysis of coupling of partial models,
- analysis of the full model by means of partial ones their couplings are considered to be weak, and thus they can be treated as perturbations of successive iterations.

In general, two types of partial models can be constructed:

- describing a certain group of vibrations caused by various structural parts of a given machine,
- describing vibrations of particular parts.

Proper choice of partial models depends on the type of particular situation and the aim of analysis [3].

A characteristic feature of the proposed method is its iterative manner of calculations. Thus the convergence of computational procedures constitutes, from the applicability point of view, the main problem to be dealt with. Such analysis with respect to linear system was made in [4] where the conditions for, and domains of, convergence of iterative procedures were determined, both for conservative and dissipative systems.

In this paper a problem of convergence in the case of nonlinear systems is considered.

## 2. FORMULATION OF THE PROBLEM

To focus our attention on the analysis of the influence of nonlinearity on the convergence of the iterative computational procedure let us assume a simple, two-mass model. Elastic characteristic of an element connecting two masses is assumed to be nonlinear, i.e. the nonlinearity is present along the decomposition line of the element. For the sake of generality, no constraints will be imposed on the type of this nonlinearity. Assume that the decomposition is made in the same manner as in the case of weak associations between masses in the complex model [2]. Let us separate from a nonlinear element (in an arbitrary manner) a linear component with the stiffness  $k_2$ , Fig. 1.

Equations for vibrations of the model have the form

$$(2.1) \quad \begin{aligned} m_1 \ddot{z}_1 + z_1(k_1 + k_2) &= k_1 z_0 + k_2 z_2 + \varphi(z_2 - z_1), \\ m_2 \ddot{z}_2 + z_2 k_2 &= k_2 z_1 - \varphi(z_2 - z_1). \end{aligned}$$

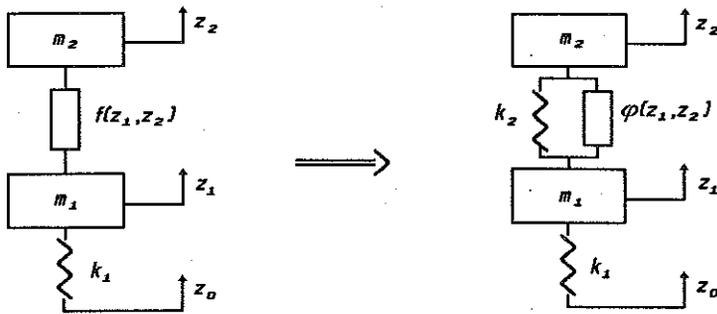


FIG. 1. Initial and transformed forms of a model.

This model will be split up into two partial models, the vibrations of the first one being expressed by Eq. (2.1)<sub>1</sub>, and of the other one by Eq. (2.1)<sub>2</sub>.

Assume that the solutions  $z_1$ ,  $z_2$  and the frequencies  $\omega_1^2$ ,  $\omega_2^2$  can be represented by power series with respect to a parameter  $\varepsilon$

$$(2.2) \quad z_1 = y_{01} + \varepsilon y_{11} + \varepsilon^2 y_{21} + \dots + \varepsilon^i y_{i1},$$

$$z_2 = y_{02} + \varepsilon y_{12} + \varepsilon^2 y_{22} + \dots + \varepsilon^i y_{i2};$$

$$(2.3) \quad \omega_1^2 = \omega_{01}^2 + \varepsilon \omega_{11}^2 + \varepsilon^2 \omega_{21}^2 + \dots + \varepsilon^i \omega_{i1}^2,$$

$$\omega_2^2 = \omega_{02}^2 + \varepsilon \omega_{12}^2 + \varepsilon^2 \omega_{22}^2 + \dots + \varepsilon^i \omega_{i2}^2,$$

and that the parameter  $\varepsilon$  is also present in the coupling terms of the first equation and in the nonlinear terms. Let us rearrange the system (2.1) as follows:

$$(2.4) \quad \ddot{z}_1 + \omega_{01}^2 z_1 = \frac{k_1}{m_1} z_0 + \frac{\varepsilon K}{m_1} z_2 + \frac{\varepsilon}{m_1} \underline{g(z_2 - z_1)},$$

$$\ddot{z}_2 + \omega_{02}^2 z_2 = \frac{k_2}{m_2} z_1 - \frac{\varepsilon}{m_2} \underline{g(z_2 - z_1)},$$

where

$$(2.5) \quad \varphi(z_2 - z_1) = \varepsilon g(z_2 - z_1)$$

and

$$(2.6) \quad k_2 = \varepsilon K.$$

The underlined terms in Eqs. (2.4) will be treated as weak couplings.

If the function  $g(z_1, z_2)$  has, in the neighbourhood of zero solutions  $y_{01}$ ,  $y_{02}$ , continuous partial derivatives up to an arbitrary order, it can be expanded into Taylor's series,

$$\begin{aligned}
 (2.7) \quad g(z_1, z_2) = & g(y_{01}, y_{02}) + \frac{\partial g}{\partial z_1}(\varepsilon y_{11} + \varepsilon^2 y_{21} + \varepsilon^3 y_{31} + \dots) \\
 & + \frac{\partial g}{\partial z_2}(\varepsilon y_{12} + \varepsilon^2 y_{22} + \dots) + \frac{1}{2} \left[ \frac{\partial^2 g}{\partial z_1^2}(\varepsilon y_{11} + \varepsilon^2 y_{21} + \dots)^2 \right. \\
 & + \frac{\partial^2 g}{\partial z_2^2}(\varepsilon y_{12} + \varepsilon^2 y_{22} + \dots)^2 + 2 \frac{\partial^2 g}{\partial z_1 \partial z_2}(\varepsilon y_{11} + \varepsilon^2 y_{21} + \dots) \\
 & \quad \left. \times (\varepsilon y_{12} + \varepsilon^2 y_{22} + \dots) \right] + \frac{1}{6} \left[ \frac{\partial^3 g}{\partial z_1^3}(\varepsilon y_{11} + \varepsilon^2 y_{21} + \dots)^3 \right. \\
 & + \frac{\partial^3 g}{\partial z_2^3}(\varepsilon y_{12} + \varepsilon^2 y_{22} + \dots)^3 + 3 \frac{\partial^3 g}{\partial z_1 \partial z_2^2}(\varepsilon y_{11} + \varepsilon^2 y_{21} + \dots) \\
 & \quad \times (\varepsilon y_{12} + \varepsilon^2 y_{22} + \dots)^2 + 3 \frac{\partial^3 g}{\partial z_1^2 \partial z_2}(\varepsilon y_{11} + \varepsilon^2 y_{21} + \dots)^2 \\
 & \quad \left. \times (\varepsilon y_{12} + \varepsilon^2 y_{22} + \dots) \right] + \dots
 \end{aligned}$$

On rearranging with respect to the powers of  $\varepsilon$ , the above expression takes the form

$$(2.8) \quad g(z_1, z_2) = g(y_{01}, y_{02}) + \varepsilon A_1 + \varepsilon^2 A_2 + \varepsilon^3 A_3 + \varepsilon^4 A_4 + \dots,$$

where

$$(2.9) \quad A_1 = \frac{\partial g}{\partial z_1} y_{11} + \frac{\partial g}{\partial z_2} y_{12},$$

$$(2.10) \quad A_2 = \frac{\partial g}{\partial z_1} y_{21} + \frac{\partial g}{\partial z_2} y_{22} + \frac{1}{2} \frac{\partial^2 g}{\partial z_1^2} y_{11}^2 + \frac{1}{2} \frac{\partial^2 g}{\partial z_2^2} y_{12}^2 + \frac{\partial^2 g}{\partial z_1 \partial z_2} y_{11} y_{12},$$

$$\begin{aligned}
 (2.11) \quad A_3 = & \frac{\partial g}{\partial z_1} y_{31} + \frac{\partial g}{\partial z_2} y_{32} + \frac{\partial^2 g}{\partial z_1^2} y_{11} y_{21} + \frac{\partial^2 g}{\partial z_2^2} y_{12} y_{22} \\
 & + \frac{\partial^2 g}{\partial z_1 \partial z_2} (y_{11} y_{22} + y_{12} y_{21}) + \frac{1}{6} \frac{\partial^3 g}{\partial z_1^3} y_{11}^3 + \frac{1}{6} \frac{\partial^3 g}{\partial z_2^3} y_{12}^3 \\
 & + \frac{1}{2} \frac{\partial^3 g}{\partial z_1 \partial z_2^2} y_{11} y_{12}^2 + \frac{1}{2} \frac{\partial^3 g}{\partial z_1^2 \partial z_2} y_{11}^2 y_{12},
 \end{aligned}$$

$$\begin{aligned}
 (2.12) \quad A_4 = & \frac{\partial g}{\partial z_1} y_{41} + \frac{\partial g}{\partial z_2} y_{42} + \frac{\partial^2 g}{\partial z_1^2} \left( y_{11} y_{31} + \frac{1}{2} y_{21}^2 \right) \\
 & + \frac{\partial^2 g}{\partial z_2^2} \left( y_{12} y_{32} + \frac{1}{2} y_{22}^2 \right) + \frac{\partial^2 g}{\partial z_1 \partial z_2} (y_{11} y_{32} + y_{12} y_{31} + y_{21} y_{22}) \\
 & + \frac{1}{2} \frac{\partial^3 g}{\partial z_1^3} y_{11}^2 y_{21} + \frac{1}{2} \frac{\partial^3 g}{\partial z_2^3} y_{12}^2 y_{22} + \frac{1}{2} \frac{\partial^3 g}{\partial z_1 \partial z_2^2} (2y_{11} y_{12} y_{22} + y_{12}^2 y_{21})
 \end{aligned}$$

$$(2.12) \quad + \frac{1}{2} \frac{\partial^3 g}{\partial z_1^2 \partial z_2} (y_{11}^2 y_{22} + 2y_{11} y_{21} y_{12}) + \frac{1}{24} \frac{\partial^4 g}{\partial z_1^4} y_{11}^4 + \frac{1}{24} \frac{\partial^4 g}{\partial z_2^4} y_{12}^4$$

[cont.]

$$+ \frac{1}{6} \frac{\partial^4 g}{\partial z_1^3 \partial z_2} y_{11}^3 y_{12} + \frac{1}{4} \frac{\partial^4 g}{\partial z_1^2 \partial z_2^2} y_{11}^2 y_{12}^2 + \frac{1}{6} \frac{\partial^4 g}{\partial z_1 \partial z_2^3} y_{11} y_{12}^3.$$

Assume that the system is acted upon by a harmonic excitation in the form

$$z_0 = Z \sin \nu t.$$

The steady vibrations of the system will be considered. Periodicity of the solution is also assumed, i.e. no secular terms of the type  $t \sin \nu t$  should appear in the solutions.

### 3. REALIZATION OF THE ITERATIVE PROCEDURE

Assume that in the  $i$ -th iteration the terms of the expansion  $g(z_1, z_2)$  into Taylor's series up to the  $i$ -th power of the parameter  $\varepsilon$  will be included, and that the  $i$ -th iteration yields an approximate solution up to the  $i$ -th power of the parameter  $\varepsilon$ . The course of the iterative procedure will be the following:

0-th iteration

$$(3.1) \quad \ddot{z}_1^{(0)} + \omega_{01}^2 z_1^{(0)} = \frac{k_1}{m_1} z_0 \quad \longrightarrow \quad z_1^{(0)} = y_{01}; \quad \omega_1^2 = \omega_{01}^2,$$

$$\ddot{z}_2^{(0)} + \omega_{02}^2 z_2^{(0)} = \frac{k_2}{m_2} z_1^{(0)} \quad \longrightarrow \quad z_2^{(0)} = y_{02}; \quad \omega_2^2 = \omega_{02}^2.$$

1-st iteration

$$(3.2) \quad \ddot{z}_1^{(1)} + \omega_{01}^2 z_1^{(1)} = \frac{k_1}{m_1} z_0 + \frac{\varepsilon K}{m_1} z_2^{(0)} + \frac{\varepsilon}{m_1} g(y_{01}, y_{02})$$

$$\quad \longmapsto \quad z_1^{(1)} = y_{01} + \varepsilon y_{11}, \quad \omega_1^2 = \omega_{01}^2 + \varepsilon \omega_{11}^2,$$

$$\ddot{z}_2^{(1)} + \omega_{02}^2 z_2^{(1)} = \frac{k_2}{m_2} z_1^{(1)} - \frac{\varepsilon}{m_2} g(y_{01}, y_{02})$$

$$\quad \longmapsto \quad z_2^{(1)} = y_{02} + \varepsilon y_{12}, \quad \omega_2^2 = \omega_{02}^2 + \varepsilon \omega_{12}^2,$$

2-nd iteration

$$(3.3) \quad \ddot{z}_1^{(2)} + \omega_{01}^2 z_1^{(2)} = \frac{k_1}{m_1} z_0 + \frac{\varepsilon K}{m_1} z_2^{(1)} + \frac{\varepsilon^2}{m_1} A_1$$

$$\quad \longmapsto \quad z_1^{(2)} = y_{01} + \varepsilon y_{11} + \varepsilon^2 y_{21}, \quad \omega_1^2 = \omega_{01}^2 + \varepsilon \omega_{11}^2 + \varepsilon^2 \omega_{21}^2,$$

$$\ddot{z}_2^{(2)} + \omega_{02}^2 z_2^{(2)} = \frac{k_2}{m_2} z_1^{(2)} - \frac{\varepsilon}{m_2} A_1$$

$$\quad \longmapsto \quad z_2^{(2)} = y_{02} + \varepsilon y_{12} + \varepsilon^2 y_{22}, \quad \omega_2^2 = \omega_{02}^2 + \varepsilon \omega_{12}^2 + \varepsilon^2 \omega_{22}^2.$$

When the solutions appearing on the right-hand side are substituted to the system of differential equations belonging to a given iteration and are ordered according to the powers of  $\varepsilon$ , a condition of satisfaction of these equations for an arbitrary value of the parameter can be replaced by a condition to fulfil the equations at suitable powers of the parameter  $\varepsilon$ .

For example, consideration of the 2-nd iteration leads so the conclusion that the system obtained for the 0-th power of  $\varepsilon$  is identical with all the other iterations starting from the 1-st one, and so on. These systems have the form:

at  $\varepsilon^0$

$$(3.4) \quad L_0 = \begin{cases} \ddot{y}_{01} + \omega_1^2 y_{01} = \frac{k_1}{m_1} z_0 \longrightarrow y_{01}, & \omega_{01}^2, \\ \ddot{y}_{02} + \omega_2^2 y_{02} = \frac{k_2}{m_2} y_{01} \longrightarrow y_{02}, & \omega_{02}^2; \end{cases}$$

at  $\varepsilon^1$

$$(3.5) \quad L_1 = \begin{cases} \ddot{y}_{11} + \omega_1^2 y_{11} = \omega_{11}^2 y_{01} + \frac{K}{m_1} y_{02} + \frac{1}{m_1} g(y_{01}, y_{02}) \longrightarrow y_{11}, & \omega_{11}^2, \\ \ddot{y}_{12} + \omega_2^2 y_{12} = \omega_{12}^2 y_{02} + \frac{k_2}{m_2} y_{11} - \frac{1}{m_2} g(y_{01}, y_{02}) \longrightarrow y_{12}, & \omega_{12}^2; \end{cases}$$

generally,

at  $\varepsilon^i$

$$(3.6) \quad L_i = \begin{cases} \ddot{y}_{i1} + \omega_1^2 y_{i1} = \frac{K}{m_1} y_{i-1,2} + \sum_{k=1}^i \omega_{k1}^2 y_{i-k,1} + \frac{1}{m_1} A_{i-1} \longrightarrow y_{i1}, & \omega_{i1}^2, \\ \ddot{y}_{i2} + \omega_2^2 y_{i2} = \frac{k_2}{m_2} y_{i1} + \sum_{k=1}^i \omega_{k2}^2 y_{i-k,2} - \frac{1}{m_2} A_{i-1} \longrightarrow y_{i2}, & \omega_{i2}^2. \end{cases}$$

In addition, in each iteration a sequence of residuals will be obtained in the form

$$(3.7) \quad R_{i+p}^{(i)} = \begin{cases} \sum_{k=p}^i \omega_{k1}^2 y_{i+p-k,1}, \\ \sum_{k=p}^i \omega_{k2}^2 y_{i+p-k,2}. \end{cases}$$

They appear by the powers  $\varepsilon^{i+p}$ , where  $p = 1, 2, \dots, i$ .

The systems of equations to be solved at consecutive steps of the iterative procedure can be expressed as follows:

0-th iteration

$$(3.8) \quad L_0 = 0;$$

1-th iteration

$$(3.9) \quad L_0 + \varepsilon L_1 + \varepsilon^2 R_2^{(1)} = 0;$$

2-nd iteration

$$(3.10) \quad L_0 + \varepsilon L_1 + \varepsilon^2 L_2 + \varepsilon^3 R_3^{(2)} + \varepsilon^4 R_4^{(2)} = 0;$$

$i$ -th iteration

$$(3.11) \quad L_0 + \varepsilon L_1 + \dots + \varepsilon^i L_i + \varepsilon^{i+1} R_{i+1}^{(i)} + \varepsilon^{i+2} R_{i+2}^{(i)} + \dots + \varepsilon^{2i} R_{2i}^{(i)} = 0.$$

The above relationships are satisfied for an arbitrary value of the parameter if

$$(3.12) \quad L_i = 0 \quad \text{for} \quad i = 0, 1, 2, \dots$$

Assume the constant term in Taylor's expansion (2.8) to vanish,

$$(3.13) \quad g(y_{01}, y_{02}) = 0$$

and the characteristic of the nonlinear element to be a function of the displacement difference  $(z_2 - z_1)$ , i.e.

$$(3.14) \quad \frac{\partial^n g}{\partial z_1^n} = (-1)^n \frac{\partial^n g}{\partial z_2^n}.$$

Introduce the following notation:

$$(3.15) \quad T = \frac{Zk_1}{m_1}, \quad U = \frac{Zk_1k_2}{m_1m_2}, \quad W = \frac{Kk_2}{m_1m_2},$$

and

$$(3.16) \quad P = \omega_2^2 - \omega_1^2, \quad R = \omega_1^2 - \nu^2, \quad S = \omega_2^2 - \nu^2.$$

Now the solution to the system  $L_0$  (relationship (3.4)) has the form

$$(3.17) \quad \begin{aligned} y_{01} &= e_{01} \sin \nu t = \frac{T}{R} \sin \nu t, & \omega_{01}^2 &= \frac{k_1 + k_2}{m_1}, \\ y_{02} &= e_{02} \sin \nu t = \frac{U}{RS} \sin \nu t, & \omega_{02}^2 &= \frac{k_2}{m_2}. \end{aligned}$$

Solution of the system  $L_1$  (3.5) leads to

$$(3.18) \quad \begin{aligned} y_{11} &= e_{11} \sin \nu t = -\frac{TW}{PRS} \sin \nu t, & \omega_{11}^2 &= -\frac{W}{P}, \\ y_{12} &= e_{12} \sin \nu t = 0, & \omega_{12}^2 &= \frac{W}{P}. \end{aligned}$$

Introducing the notation

$$(3.19) \quad \frac{\partial g}{\partial z_2} = g'$$

to solve the system  $L_2$ , remembering the relation (3.14) and adopting a coefficient  $N_1$  (in the case  $N_1 = 1$ ), we can, in accordance with Eq. (2.9), write down

$$(3.20) \quad A_1 = N_1 g' (y_{12} - y_{11}).$$

The solution to the system  $L_2$  is

$$(3.21) \quad \begin{aligned} y_{21} &= e_{21} \sin \nu t = -\frac{TW}{P^2 RS} X_{11} \sin \nu t, & \omega_{21}^2 &= -\frac{W}{P^2} X_{11}, \\ y_{22} &= e_{22} \sin \nu t = 0, & \omega_{22}^2 &= \frac{W}{P^2} X_{12}, \end{aligned}$$

where

$$(3.22) \quad X_{11} = \frac{W}{P} + \frac{N_1 g'}{m_1},$$

$$(3.23) \quad X_{12} = \frac{N_1 g' P}{k_2} + X_{11}.$$

Accounting for Eqs. (3.14), (3.19) and denoting

$$(3.24) \quad g'' = \frac{\partial^2 g}{\partial z_2^2} = \frac{\partial^2 g}{\partial z_1^2} = -\frac{\partial^2 g}{\partial z_1 \partial z_2}$$

the relationship (2.10) can be written down in the form

$$(3.25) \quad A_2 = g' (y_{22} - y_{21}) + \frac{1}{2} g'' (y_{12} - y_{11})^2.$$

Assume that

$$(3.26) \quad \frac{1}{2} g'' (y_{12} - y_{11})^2 \leq (N_2 - 1) g' (y_{22} - y_{21})$$

what means that

$$(3.27) \quad A_2 \leq N_2 g' (y_{22} - y_{21})$$

and, instead of  $A_2$  let us insert into the system  $L_3$  the right-hand side of the above inequality. This means that a system with stronger perturbation will be analysed. When such a procedure turns out to be convergent, the procedure for the system  $L_3$  with weaker perturbation  $A_2$  will also be convergent. The value of the coefficient  $N_2$  in (3.27) will be derived from the convergence condition of the procedure.

On replacing the expression  $A_2$  by the right-hand side of the inequality (3.27), the solution of the system  $L_3$  yields

$$(3.28) \quad \begin{aligned} y_{31} &= e_{31} \sin \nu t = -\frac{TW}{P^3 RS} X_{11} X_{21} \sin \nu t, & \omega_{31}^2 &= -\frac{W}{P^3} X_{11} X_{21}, \\ y_{32} &= e_{32} \sin \nu t = 0, & \omega_{32}^2 &= \frac{W}{P^3} X_{11} X_{22}, \end{aligned}$$

where

$$(3.29) \quad X_{21} = \frac{2W}{P} + \frac{N_2 g'}{m_1},$$

$$(3.30) \quad X_{22} = \frac{N_2 g' P}{k_2} + X_{21}.$$

Remembering Eqs. (3.14), (3.19), (3.24) and denoting

$$(3.31) \quad g''' = \frac{\partial^3 g}{\partial z_2^3} = -\frac{\partial^3 g}{\partial z_1^3} = \frac{\partial^3 g}{\partial z_1^2 \partial z_2} = -\frac{\partial^3 g}{\partial z_1 \partial z_2^2},$$

the relationship (2.11) for  $A_3$  takes the form

$$(3.32) \quad A_3 = g'(y_{32} - y_{31}) + g''(y_{22} - y_{21})(y_{12} - y_{11}) + g'''(y_{12} - y_{11})^3.$$

Assume that

$$(3.33) \quad g''(y_{22} - y_{21})(y_{12} - y_{11}) + g'''(y_{12} - y_{11})^3 \leq (N_3 - 1)g'(y_{32} - y_{31}),$$

that is

$$(3.34) \quad A_3 \leq N_3 g'(y_{32} - y_{31}),$$

and, similarly as before, instead of  $A_3$  let us insert to the system  $L_4$  the right-hand side of the above inequality. This means that the considered system will also be subject to some stronger perturbations.

Solving the successive systems  $L_5, L_6, \dots$ , we proceed in an analogous manner, i.e. instead of the expression  $A_{i-1}$  entering the system  $L_i$  we substitute the expression

$$(3.35) \quad A_{i-1} = N_{i-1} g'(y_{i-1,2} - y_{i-1,1}).$$

Finally, the solution in the  $i$ -th iteration has the form

$$(3.36) \quad \begin{aligned} z_1^{(i)} &= (e_{01} + \varepsilon e_{11} + \varepsilon^2 e_{21} + \dots + \varepsilon^i e_{i1}) \sin \nu t, \\ z_2^{(i)} &= (e_{02} + \varepsilon e_{12} + \varepsilon^2 e_{22} + \dots + \varepsilon^i e_{i2}) \sin \nu t, \end{aligned}$$

and the frequencies  $\omega_1^2, \omega_2^2$  are given by Eq. (2.3).

The values of the expressions  $e_{i1}, e_{i2}, \omega_{i1}^2, \omega_{i2}^2$  and the values of the ratios of the two consecutive expressions for a number of initial iterations are given in Table 1.

Table 1.

$i$	$\omega_{i1}^2$	$e_{i1}$	$\frac{\omega_{i+1,1}^2}{\omega_{i1}^2} = \frac{e_{i+1,1}}{e_{i1}}$	$\omega_{i2}^2$	$e_{i2}$	$\frac{\omega_{i+1,2}^2}{\omega_{i2}^2}$
0	$\frac{k_1 + k_2}{m_1}$	$\frac{T}{R}$	—	$\frac{k_2}{m_2}$	$\frac{U}{RS}$	—
1	$-\frac{W}{P}$	$-\frac{TW}{PRS}$	—	$\frac{W}{P}$	0	—
2	$-\frac{W}{P^2} X_{11}$	$-\frac{TW}{P^2 RS} X_{11}$	$\frac{X_{11}}{P}$	$\frac{W}{P^2} X_{12}$	0	$\frac{X_{12}}{P}$
3	$-\frac{W}{P^3} X_{11} X_{21}$	$-\frac{TW}{P^3 RS} X_{11} X_{21}$	$\frac{X_{21}}{P}$	$\frac{W}{P^3} X_{11} X_{22}$	0	$\frac{X_{11} X_{22}}{P X_{12}}$
4	$-\frac{W}{P^4} X_{11} X_{21} X_{31}$	$-\frac{TW}{P^4 RS} X_{11} X_{21} X_{31}$	$\frac{X_{31}}{P}$	$\frac{W}{P^4} X_{11} X_{21} X_{32}$	0	$\frac{X_{21} X_{32}}{P X_{22}}$
$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$

The magnitudes  $T, U, W, P, R, S$  in Table 1 are determined by the relations (3.15) and (3.16);  $X_{11}, X_{21}, X_{12}, X_{22}$  by the relations (3.22), (3.23), (3.29), (3.30), respectively.

In addition

$$(3.37) \quad X_{31} = \frac{2W}{P} + \frac{WX_{11}}{PX_{21}} + \frac{N_3 g'}{m_1}, \quad X_{32} = \frac{N_3 g' P}{k_2} + X_{31},$$

$$(3.38) \quad X_{41} = \frac{2W}{P} + \frac{2WX_{11}}{PX_{31}} + \frac{N_4 g'}{m_1}, \quad X_{42} = \frac{N_4 g' P}{k_2} + X_{41}.$$

## 4. CONVERGENCE CONDITIONS FOR THE PROCEDURE

## 4.1. General criteria of convergence

The iterative procedure for solving the system (2.4) will be convergent provided the series of coefficients shown in Table 1 will also be convergent. It can be seen that for  $e_{i1}$  and  $\omega_{i1}^2$  the ratio of the next term to the given one is the same, so that the convergence condition of these series will be also the same. Identical series, but shifted by one iteration, appears in the expressions for  $\omega_{i2}^2$ .

In order to prove the convergence of those solutions let us assume that there exists such an  $X_1$  that

$$(4.1) \quad \left| \frac{X_1}{P} \right| \leq 1$$

and

$$(4.2) \quad X_1 \geq X_{i1} \quad \text{for} \quad i = 1, 2, 3, \dots$$

When the coefficients  $N_i$  will be equal to

$$(4.3) \quad N_1 = \frac{1}{1}, \quad N_2 = \frac{2}{1}, \quad N_3 = \frac{5}{2}, \quad N_4 = \frac{14}{5}, \quad N_5 = \frac{42}{14}, \dots$$

then the expressions  $X_{k1}$  will attain the values given in Table 2.

Table 2.

$N_k$	$X_{k1}$	$X_{k2}$
$N_1 = \frac{1}{1}$	$X_{11} = \frac{W}{P} + \frac{g'}{m_1}$	$X_{12} = \frac{g'P}{k_2} + X_{11}$
$N_2 = \frac{2}{1}$	$X_{21} = 2X_{11}$	$X_{22} = 2X_{12}$
$N_3 = \frac{5}{2}$	$X_{31} = \frac{5}{2}X_{11}$	$X_{32} = \frac{5}{2}X_{12}$
$N_4 = \frac{14}{5}$	$X_{41} = \frac{14}{5}X_{11}$	$X_{42} = \frac{14}{5}X_{12}$
$\vdots$	$\vdots$	$\vdots$

The ratios of the two consecutive coefficients appearing in the solutions (Table 1) will have in the case considered the values

$$(4.4) \quad \frac{1X_{11}}{1P}, \quad \frac{2X_{11}}{1P}, \quad \frac{5X_{11}}{2P}, \quad \frac{14X_{11}}{5P}, \quad \frac{42X_{11}}{14P}, \dots$$

They constitute a series whose terms are products of  $X_{11}/P$  and the numerical series  $N_i$  (relationship (4.3)). Convergence of the iteration procedure depends on the properties of this series. If it turns out to be divergent, then the ratios of the two consecutive coefficients appearing in the solutions would be larger and larger, thus the series constituting the solutions (relations (3.36) and (2.3)) would be divergent.

A pattern of creation of this series is presented in Table 3.

Table 3.

iter.								$\Sigma$	$i$
2	1 × 1							1	1
3	1 × 1    1 × 1							2	2
4	2 × 1    1 × 1    1 × 2							5	3
5	5 × 1    2 × 1    1 × 2    1 × 5							14	4
6	14 × 1    5 × 1    2 × 2    1 × 5    1 × 14							42	5
7	42 × 1    14 × 1    5 × 2    2 × 5    1 × 14    1 × 42							132	6
8	132 × 1	42 × 1	14 × 2	5 × 5	2 × 14	1 × 42	1 × 132	429	7
⋮	⋮							⋮	⋮

The values of the terms  $N_i$  are determined by the following recurrence formula:

$$(4.5) \quad N_i = \frac{a_i}{a_{i-1}}, \quad i = 1, 2, 3, \dots,$$

where

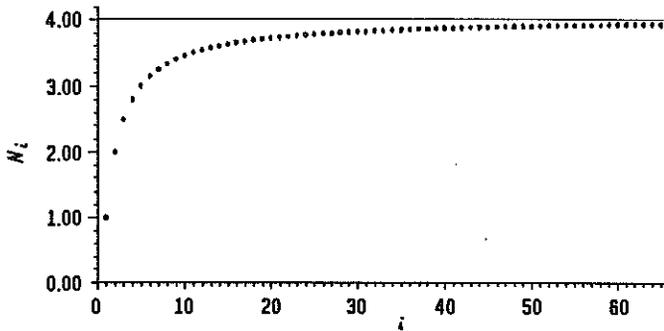
$$(4.6) \quad a_0 = 1, \quad a_i = \sum_{k=0}^{i-1} a_k a_{i-k-1}, \quad i = 1, 2, \dots$$

This series is finite – see Fig. 2 – and its terms satisfy the condition

$$(4.7) \quad N_i < 4, \quad i = 1, 2, \dots$$

Thus the series (4.4) possesses a majorant in the form of a geometric series with the quotient

$$(4.8) \quad q = \frac{4X_{11}}{P}$$

FIG. 2. Series  $N_i$  (relation (4.5)).

This means that the sought expression  $X_1$  (relation (4.1)) is determined as

$$(4.9) \quad X_1 = 4X_{11}.$$

For the series of coefficients obtained in the  $i$ -th iteration of the solution  $z_1$  (relation (3.36)), the majorant has the form

$$(4.10) \quad e_{01} + \varepsilon e_{11} + \varepsilon e_{11}(\varepsilon q) + \varepsilon e_{11}(\varepsilon q)^2 + \dots + \varepsilon e_{11}(\varepsilon q)^i.$$

For the frequencies  $\omega_1^2$ ,  $\omega_2^2$  (relation (2.3)) similar series can be formed by majoring them.

The convergence condition for all these series is

$$(4.11) \quad |\varepsilon q| < 1.$$

On substituting here Eq. (3.22) and taking account of Eq. (2.5), we get

$$(4.12) \quad \left| \frac{4\varepsilon W}{P^2} + \frac{4\varphi'}{Pm_1} \right| < 1.$$

Making use of Eqs. (3.15) and (3.16) it can be concluded that the first term of the left-hand side of the above expression is recognized as Mandelstam's coefficient, which for the linear part of the system is determined by [1, 5].

$$(4.13) \quad \frac{4\varepsilon W}{P^2} = \sigma^2.$$

Thus the condition (4.12) can be finally rewritten to take the form

$$(4.14) \quad \left| \sigma^2 + \frac{4\varphi'}{Pm_1} \right| < 1.$$

The obtained form of the convergence condition for the iterative procedure makes it possible to formulate two important general conclusions:

1. The convergence criterion of the procedure for nonlinear systems contains a term  $\sigma^2$  which indicates that the satisfaction of the convergence conditions by the linear part of the system is desirable, although not necessary. In addition, a term is present that imposes certain constraints on the value of the first derivative of the nonlinear part.

2. In some cases the convergence of the iterative procedure of the analysis of nonlinear system is possible even if its separated linear part remains divergent, i.e. when the second term in the condition (4.14) causes a decrease in  $|\sigma^2|$ .

#### 4.2. Conditions referring to the first derivative of the nonlinear function $\varphi(z_1, z_2)$

Let us analyse what conditions for the first derivative of the nonlinear elastic characteristic  $\varphi'$  are imposed by satisfying of the convergence condition of the iterative procedure.

On denoting

$$(4.15) \quad G_1(S_1, S_3) = \frac{(S_1 - S_3 - S_1 S_3)^2 - 4S_1^2 S_3}{4S_1 S_3 (S_1 - S_3 - S_1 S_3)},$$

$$(4.16) \quad G_2(S_1, S_3) = \frac{-(S_1 - S_3 - S_1 S_3)^2 - 4S_1^2 S_3}{4S_1 S_3 (S_1 - S_3 - S_1 S_3)},$$

where

$$(4.17) \quad S_1 = \frac{k_2}{k_1}, \quad S_3 = \frac{m_2}{m_1},$$

and

$$(4.18) \quad \varphi' = \frac{d\varphi}{d\lambda}$$

as well as

$$(4.19) \quad \lambda = z_2 - z_1,$$

the condition (4.14) generates the following constraints on  $\varphi'$ , depending on the parameters  $S_1$  and  $S_3$  of the system and on the stiffness  $k_2$  of the separated linear part:

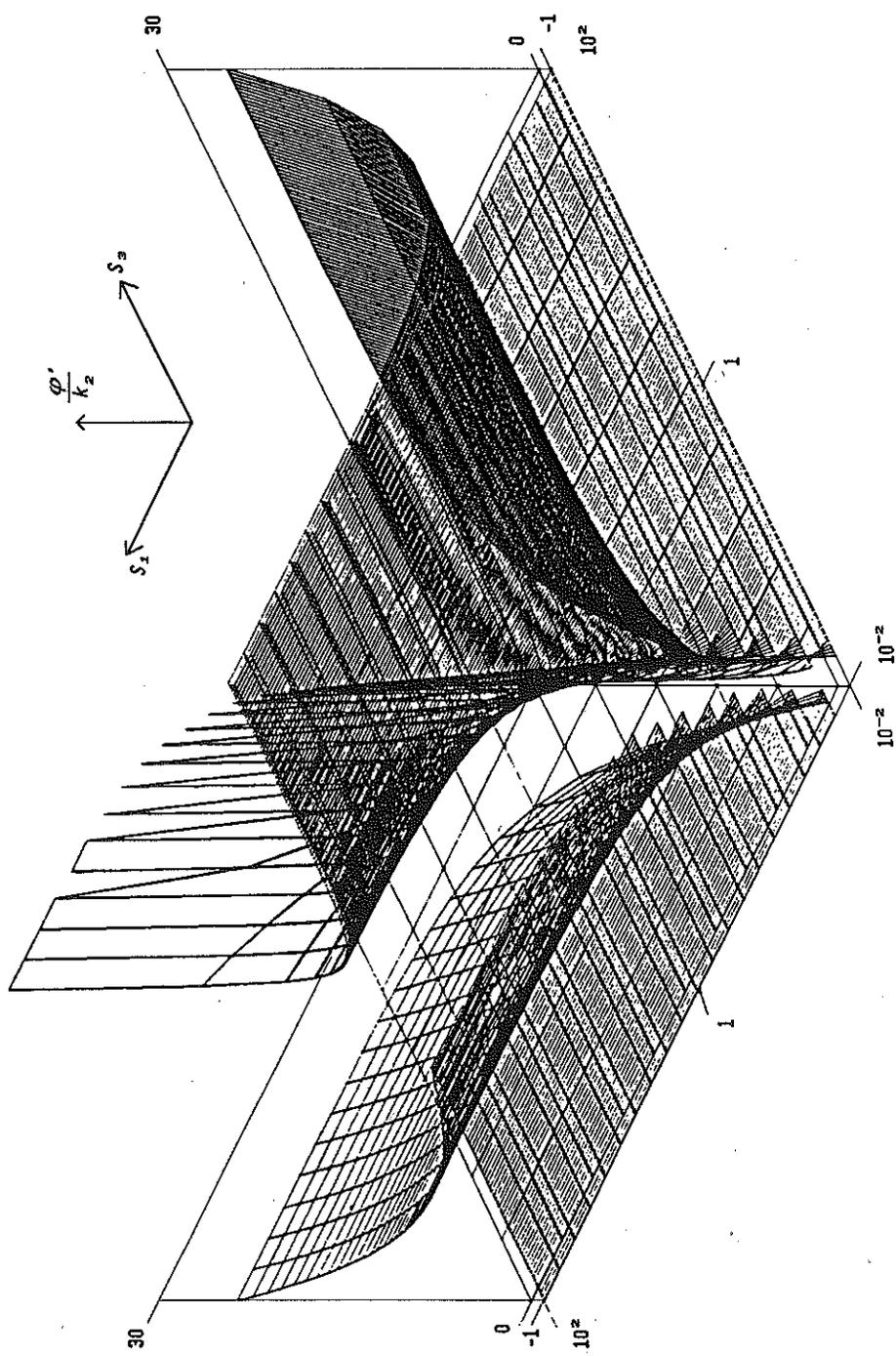


FIG. 3. Admissible domains of variability of the ratio  $\varphi/k_2$ .

a) for  $P < 0$ , i.e.  $\omega_2 < \omega_1$

$$(4.20) \quad G_1(S_1, S_3) < \frac{\varphi'}{k_2} < G_2(S_1, S_3),$$

b) for  $P > 0$ , i.e.  $\omega_2 > \omega_1$

$$(4.21) \quad G_2(S_1, S_3) < \frac{\varphi'}{k_2} < G_1(S_1, S_3).$$

It should be remembered that the condition

$$(4.22) \quad \frac{\varphi'}{k_2} > -1$$

has to be met, otherwise a zero or even negative stiffness would exist between the masses  $m_1$  and  $m_2$ .

The conditions (4.20)–(4.22) are shown in Fig.3.

### 4.3. Conditions referring to the second derivative of the function $\varphi(z_1, z_2)$

Although the condition (4.14) analysed above imposes explicitly the constraints on the first derivative of the nonlinear function  $\varphi(\lambda)$  only, the values of the higher order derivatives have by no means been ignored in the considerations. These conditions result from certain additional assumptions made in the course of analysis, namely Eqs. (3.26), (3.33) and (3.35).

According to the relationships (3.26) and (4.3)<sub>2</sub> we can write

$$(4.23) \quad g'' \leq 2g' \frac{(y_{22} - y_{21})}{(y_{12} - y_{11})^2}.$$

For  $\varepsilon > 0$  the above inequality, in accordance with Eq. (2.5), is equivalent to the inequality

$$(4.24) \quad \varphi'' \leq 2\varphi' \frac{(y_{22} - y_{21})}{(y_{12} - y_{11})^2}.$$

Substituting into (4.24) the values of coefficients of the solutions given in Table 1 and rearranging, we get the condition for the second derivative of the function  $\varphi(\lambda)$ :

$$(4.25) \quad \varphi'' \leq 2\varphi' \frac{\frac{\varepsilon W}{P^2} + \frac{\varphi'}{m_1 P}}{\varepsilon y_{11}}.$$

The right-hand side of this inequality is a quadratic polynomial with respect to  $\varphi'$  and has the roots:

$$(4.26) \quad \varphi'_1 = 0, \quad \varphi'_2 = k_2 G_3(S_1, S_3),$$

where

$$(4.27) \quad G_3(S_1, S_3) = \frac{S_1}{S_1 S_3 + S_3 - S_1}.$$

The condition (4.25) is shown diagrammatically in Figs. 4 and 5. The domains of admissible values of the second derivative of  $\varphi'$  are shaded. Moreover, the lines are shown indicating the convergence limits of the procedures:  $G_2 k_2$  for  $P < 0$  (Fig. 4) and  $G_1 k_2$  for  $P > 0$  (Fig. 5), in conformity with the relations visualized in Fig. 3. In this figure we can also see that only for very small values of  $S_1$  or  $S_3$  – i.e. for those cases in which the iterative analysis of the linear part would be convergent very rapidly – a larger range

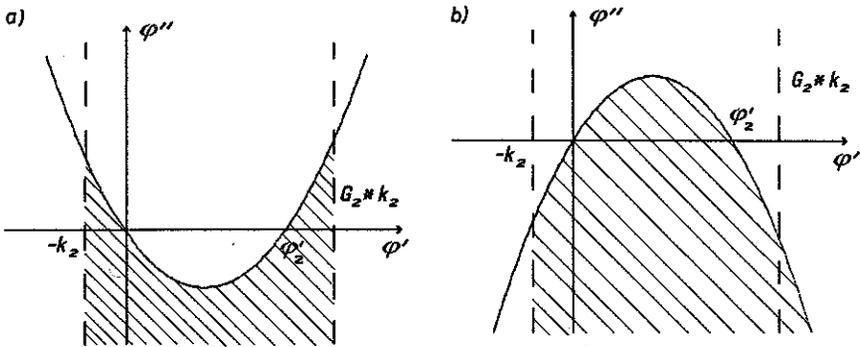


FIG. 4. Diagram of the relation (4.25) for  $P < 0$  ( $\omega_2 < \omega_1$ ). a)  $y_{11} > 0$ ; b)  $y_{11} < 0$ .

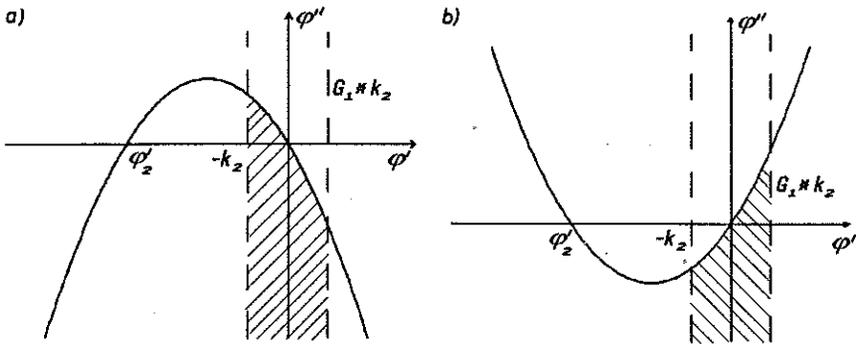


FIG. 5. Diagram of the relation (4.25) for  $P > 0$  ( $\omega_2 > \omega_1$ ). a)  $y_{11} > 0$ ; b)  $y_{11} < 0$ .

of changes in the first derivative  $\varphi'$  is allowable. For the greater part of the remaining cases the intervals  $(-1, G_2k_2)$  or  $(-1, G_1k_2)$  are very narrow and the values  $G_1k_2, G_2k_2, G_3k_2$  differ very little. In view of this fact, Figs. 4 and 5 show that in the majority of cases the convergence procedure requires the second derivative to be negative (regressive characteristic).

## 5. FINAL REMARKS

The conditions regarding higher order derivatives of the nonlinear characteristic  $\varphi(\lambda)$  can be derived in a similar way. For instance, the relationships (3.33), (4.3) and suitable expressions from Table 1 supply, after some rearrangements, the condition for the third derivative

$$\varphi''' y_{11}^3 \geq 9\varphi' y_{31} + 6\varphi'' y_{11} y_{21}.$$

Basing on the relation (3.35), the conditions can be formulated referring to higher order derivatives. However, their form becomes more complex and they are functions of the lower order derivatives, so their analysis is excessively complicated. That is why it is reasonable to terminate the analysis on lower order derivatives only.

It is interesting to realize that the presented results can be used to "synthesize" certain nonlinear characteristic ensuring the iterative convergence of the analysis of the complete system with given parameters.

During derivation of the convergence conditions presented in this paper, an assessment from above was made repeatedly (e.g. the series  $N_i$ , use of the majorant and others), thus the actual convergence conditions are less stringent than those presented.

The problem of the convergence of the iterative procedures for nonlinear systems can be approached in two ways:

- without specifying the type of nonlinearity, to analyse the problem of convergence in order to formulate general criteria for the nonlinear characteristics to ensure their convergence;
- assuming certain typical forms of nonlinear characteristics, to examine which of them ensure the convergence of the procedures or analyze what changes are caused in the convergence domains (their narrowing or expanding) for linear systems by the introduction of a given nonlinearity.

The analysis made in this paper belongs to the first type of approach to the convergence problems of nonlinear systems. The other approach will be tackled in a separate paper.

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